

# Control Systems I

## Recitation 12

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# Last Week

## Frequency-Domain Specifications

- **Disturbance Rejection** ( $Y(s) = S(s)D(s)$ ,  $S(s)$  small)

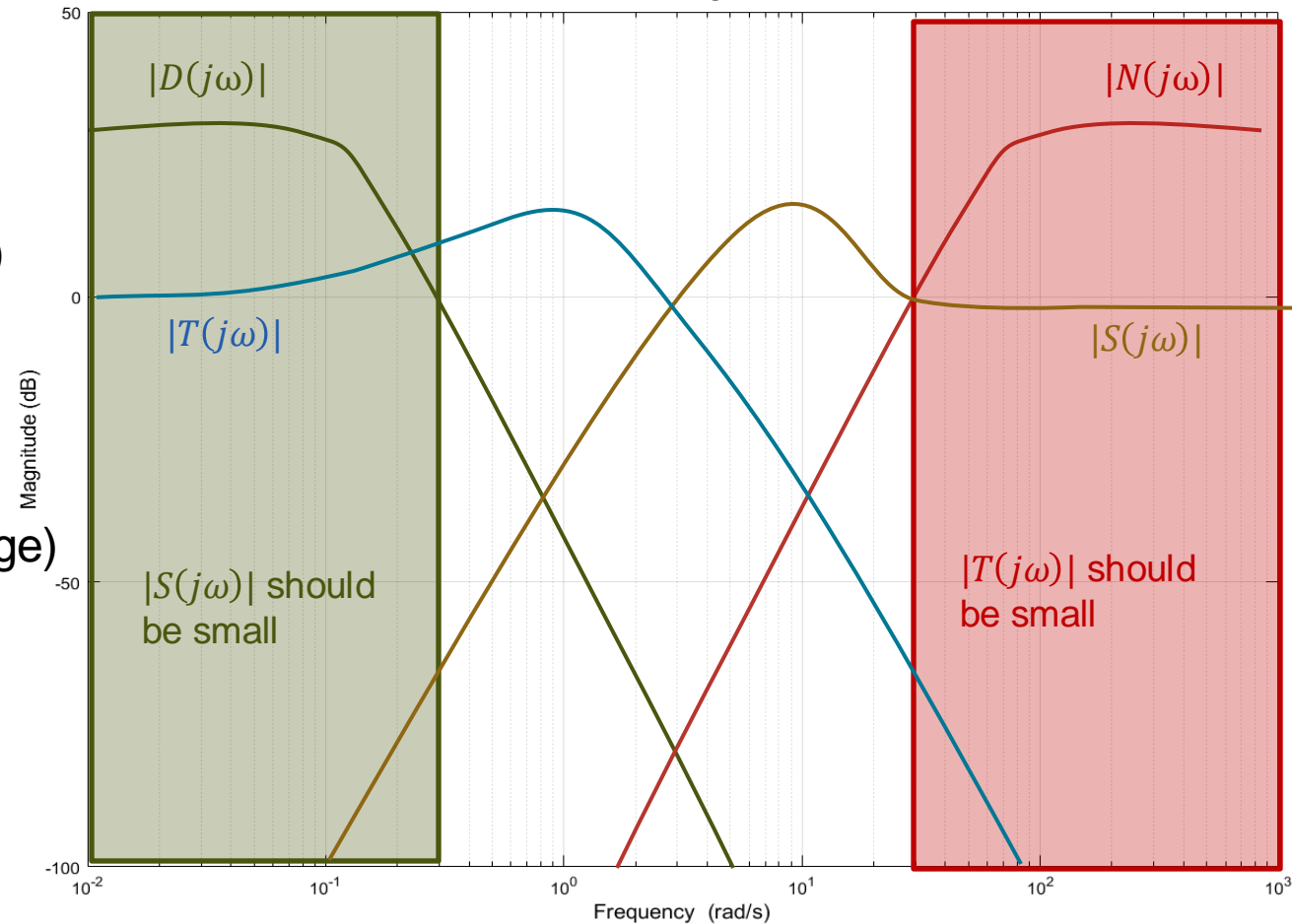
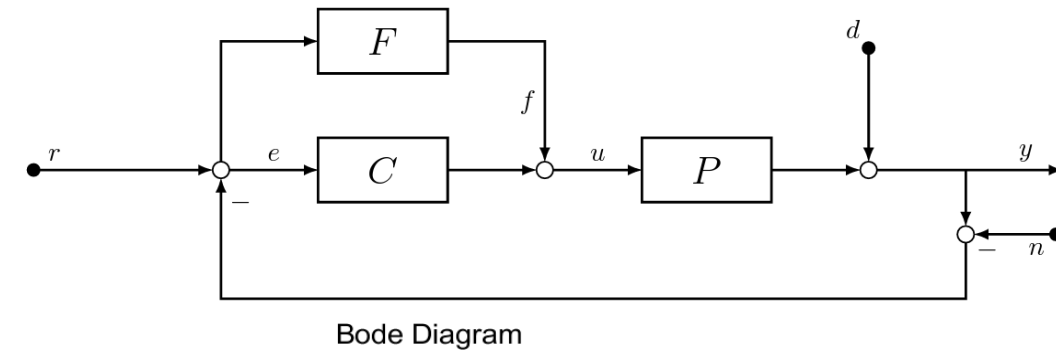
- $S(s)$  only needs to be small up to  $\omega_d$
- $T(s)$  must then be 1 in that region

- **Noise Rejection** ( $Y(s) = S(s)N(s)$ ,  $T(s)$  small)

- $T(s)$  only needs to be small after  $\omega_n$
- $S(s)$  must then be 1 in that region

- **Reference Tracking** ( $Y(s) = T(s)R(s)$ ,  $T(s)$  large)

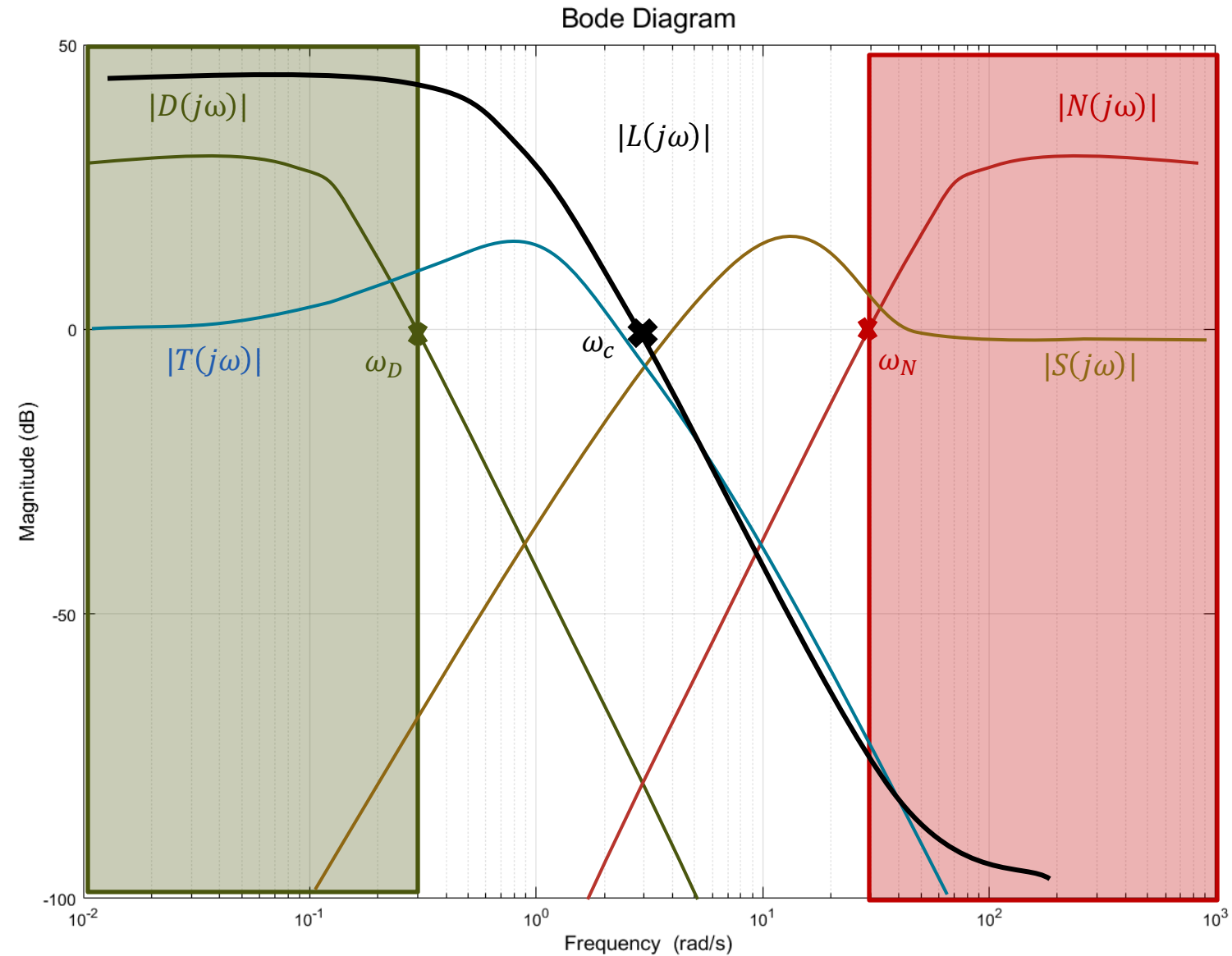
- For free from disturbance rejection



# Last Week

## Frequency-Domain Specifications

- For  $|S(j\omega)| \ll 1$ 
  - $\Rightarrow \left| \frac{1}{1+L(j\omega)} \right| \ll 1 \Rightarrow |L(j\omega)| \gg 1$
- For  $|T(j\omega)| \ll 1$ 
  - $\Rightarrow \left| \frac{L(j\omega)}{1+L(j\omega)} \right| \ll 1 \Rightarrow |L(j\omega)| \ll 1$

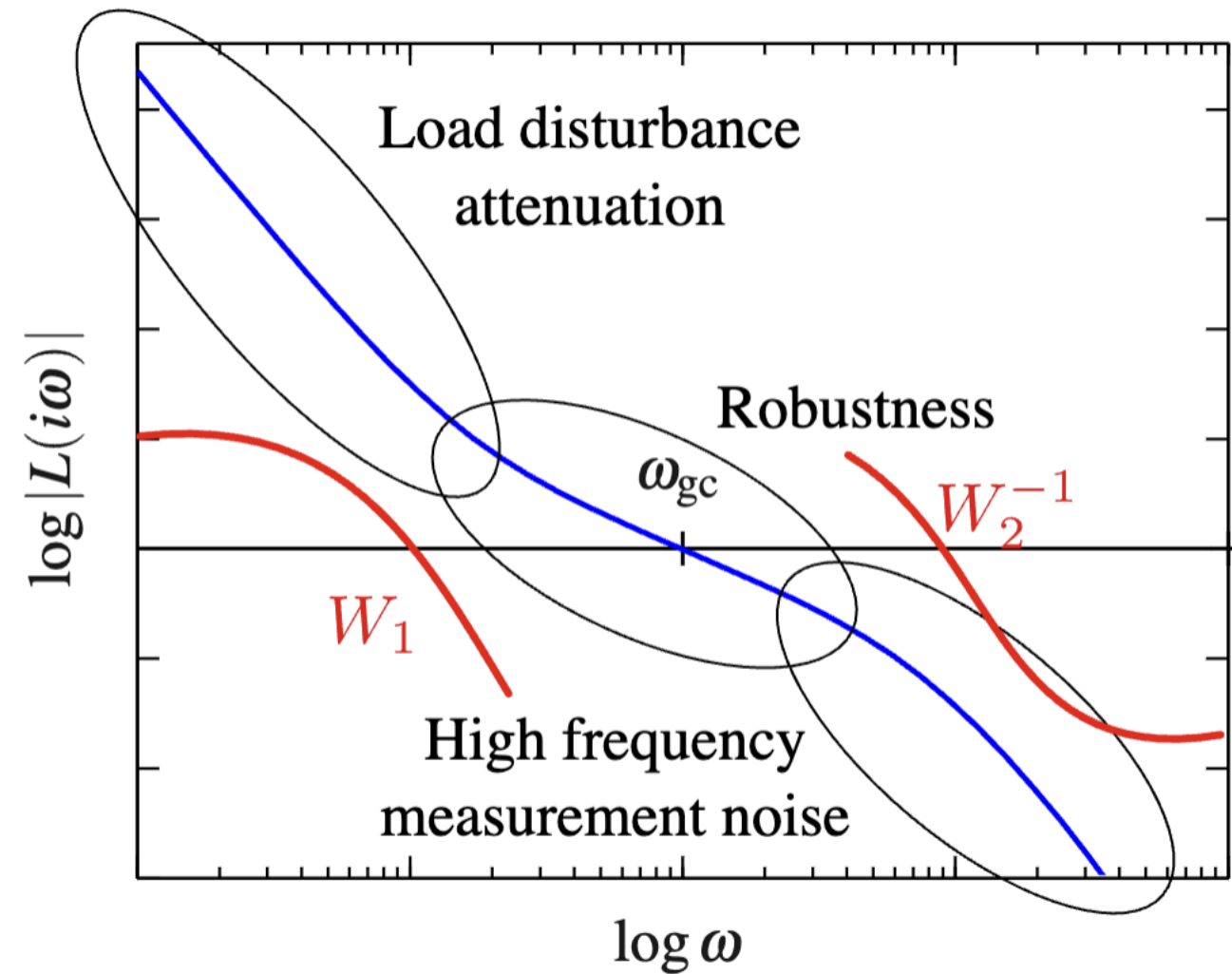




# Last Week

## Frequency-Domain Specifications

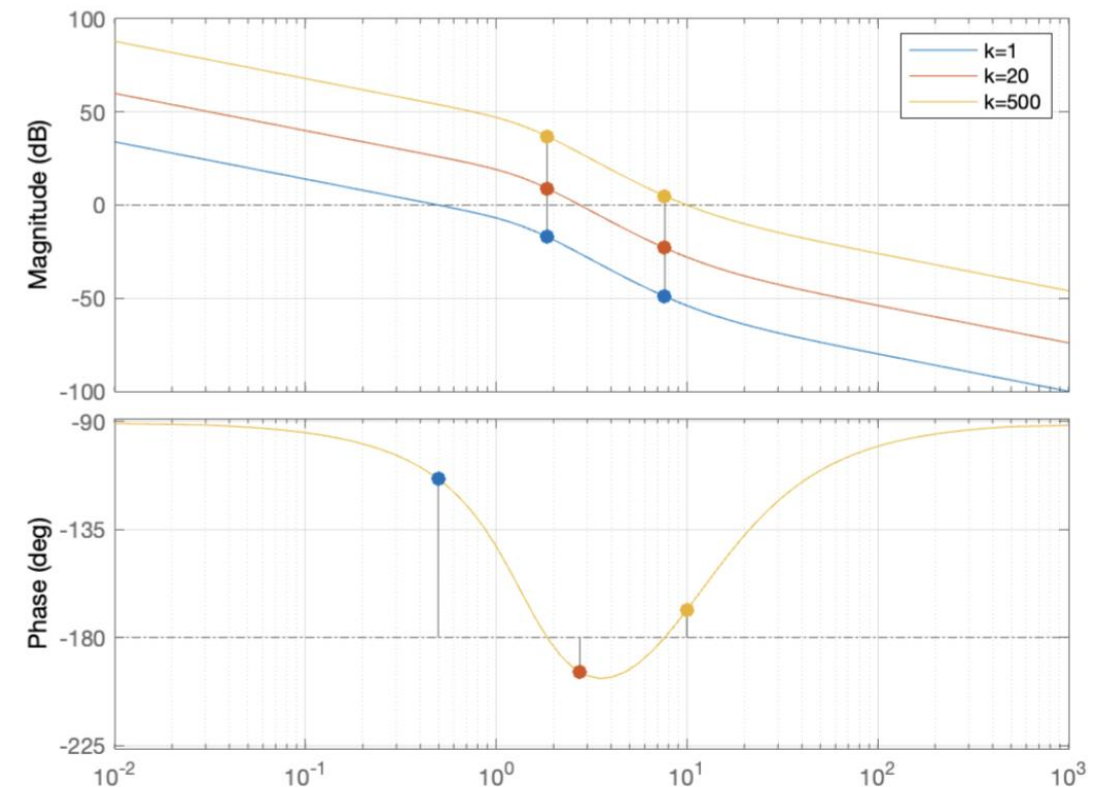
- For  $|S(j\omega)| \ll 1$ 
  - $\Rightarrow \left| \frac{1}{1+L(j\omega)} \right| \ll 1 \Rightarrow |L(j\omega)| \gg 1$
  - $|L(j\omega)| > |W_1(j\omega)|$
- For  $|T(j\omega)| \ll 1$ 
  - $\Rightarrow \left| \frac{L(j\omega)}{1+L(j\omega)} \right| \ll 1 \Rightarrow |L(j\omega)| \ll 1$
  - $|L(j\omega)| < |W_2^{-1}(j\omega)|$



# Last Week

## Loop Shaping

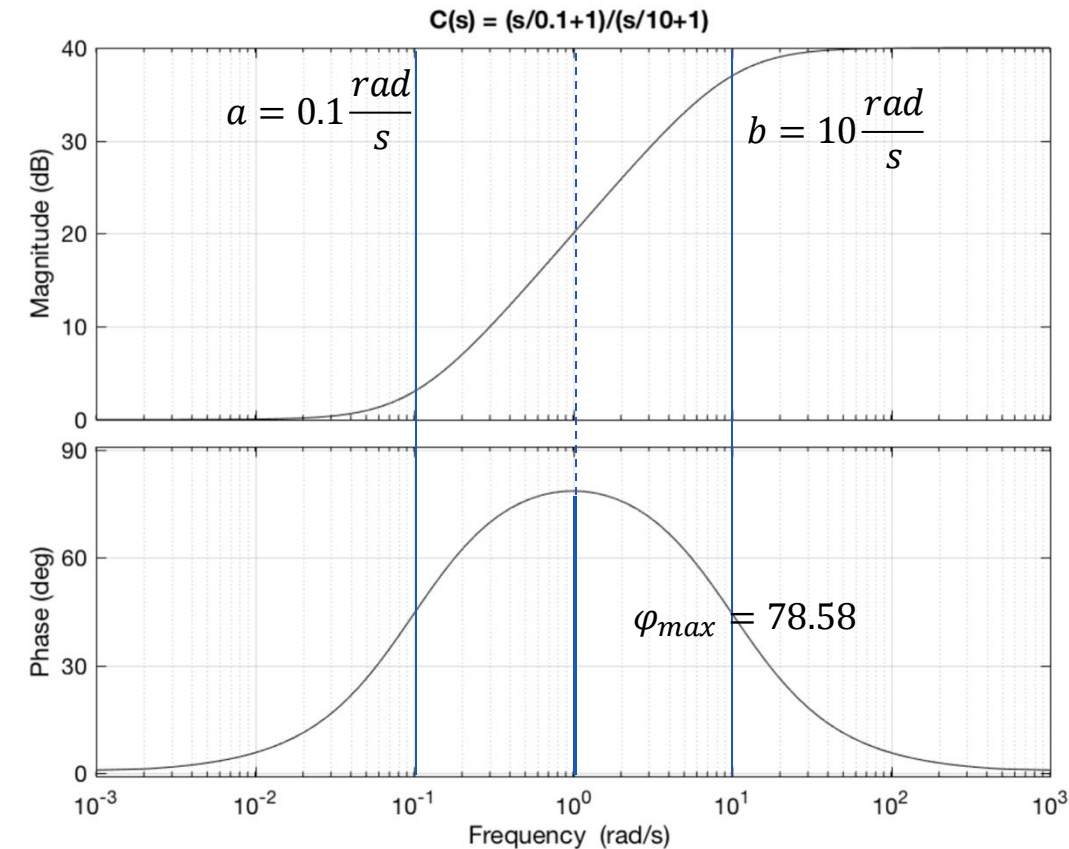
- What can we do better?
  - Use our knowledge and choose a combination of the following elements
  - Gain:  $k$ , Integrator:  $1/s$ , Lead:  $\frac{s/a+1}{s/b+1}$  ( $0 < a < b$ ), Lag:  $\frac{s/a+1}{s/b+1}$  ( $0 < b < a$ )
- **Gain:  $k$** 
  - Shifts the Magnitude Diagram up or down
  - Phase stays constant
- User Guide:
  - Move system up or down as desired
- **Integrator:  $1/s$** 
  - Gets rid of steady state error
  - $|L(0)| \rightarrow \infty$
- User Guide:
  - Add as many integrators as needed to get rid of the steady state error (beware of phase)



# Last Week

## Loop Shaping

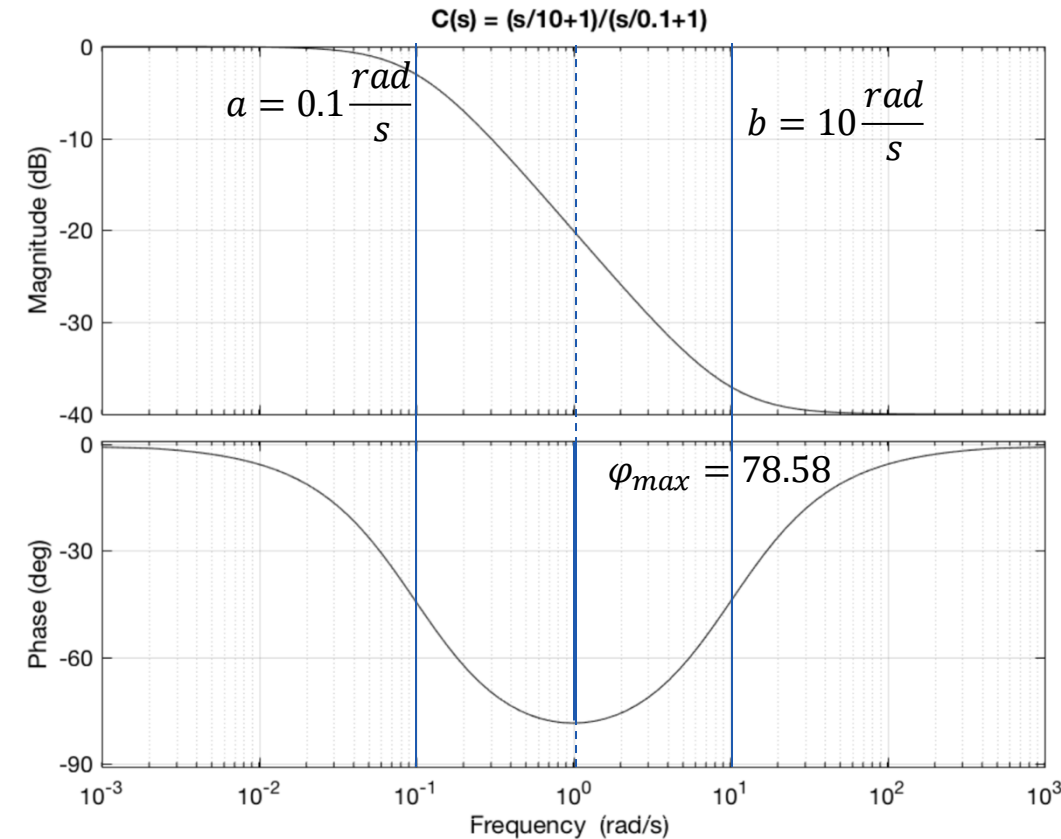
- **Lead:**  $\frac{s/a+1}{s/b+1} = \frac{b}{a} \frac{s+a}{s+b}$  ( $0 < a < b$ ), PD-Controller for  $b \rightarrow \infty$ 
  - Increases magnitude by  $b/a$  at high frequencies
  - Creates a slope of  $20 \frac{dB}{dec}$  between  $a$  and  $b$
  - Increases the phase at  $\sqrt{ab}$  (midpoint of  $[a, b]$ ) by:
    - $\varphi_{max} = 2\arctan(\sqrt{b/a}) - 90^\circ$
- User guide:
  - Used to increase the phase margin
  - Pick desired crossover frequency  $\sqrt{ab}$
  - Pick  $b/a$  for desired phase shift ( $b/a \uparrow \rightarrow \varphi \uparrow$ )
  - Use a gain  $k$  to shift crossover frequency
- Danger:
  - Increases magnitude at high frequencies -> Sensitive to noise



# Last Week

## Loop Shaping

- **Lag:**  $\frac{s/a+1}{s/b+1} = \frac{b}{a} \frac{s+a}{s+b}$  ( $0 < b < a$ ), PI-Controller for  $b \rightarrow 0$ 
  - Decreases magnitude by  $b/a$  at high frequencies
  - Creates a slope of  $-20 \frac{dB}{dec}$  between  $a$  and  $b$
  - Decreases the phase at  $\sqrt{ab}$  (midpoint of  $[a, b]$ ) by:
    - $\varphi_{max} = 2\arctan(\sqrt{b/a}) - 90^\circ$
- User guide:
  - Used to improve disturbance rejection/ref tracking
  - Pick  $a$  small enough to not affect  $\omega_c$  and  $\varphi_{margin}$ 
    - For this  $a \ll \omega_c$
- Danger:
  - Phase lag at small frequencies -> reduction of phase margin



# Last Week

## Loop Shaping

- Split System:  $P(s) = P_{mp}(s) D(s)$ 
  - $P(s) = \frac{s-z}{s-p} = \frac{s+z}{s+p} \cdot \frac{s+p}{s-p} \cdot \frac{s-z}{s+z}$
- Non-minimumphase zero:  $D(s) = -\frac{s-z}{s+z} \rightarrow \angle D(j\omega) = -2 \arctan\left(\frac{\omega}{z}\right)$ 
  - At  $\omega_c$  the system lags  $-2 \arctan\left(\frac{\omega_c}{z}\right)$
  - Nmp zeros force the system to be slow as max gain and crossover frequency are reduced
    - Slow (small  $z$ ) nmp zeros are worse than fast (large  $z$ ) ones
- Unstable pole:  $D(s) = \frac{s+zp}{s-p} \rightarrow \angle D(j\omega) = -2 \arctan\left(\frac{p}{\omega}\right)$ 
  - At  $\omega_c$  the system lags  $-2 \arctan\left(\frac{p}{\omega_c}\right)$
  - Unstable poles force the system to be faster as min gain and crossover frequency are increase
    - Slow (small  $p$ ) poles are better than fast (large  $p$ ) ones
    - Fast system requires strong and fast controllers/ actuators



# Last Week

## Performance Limits

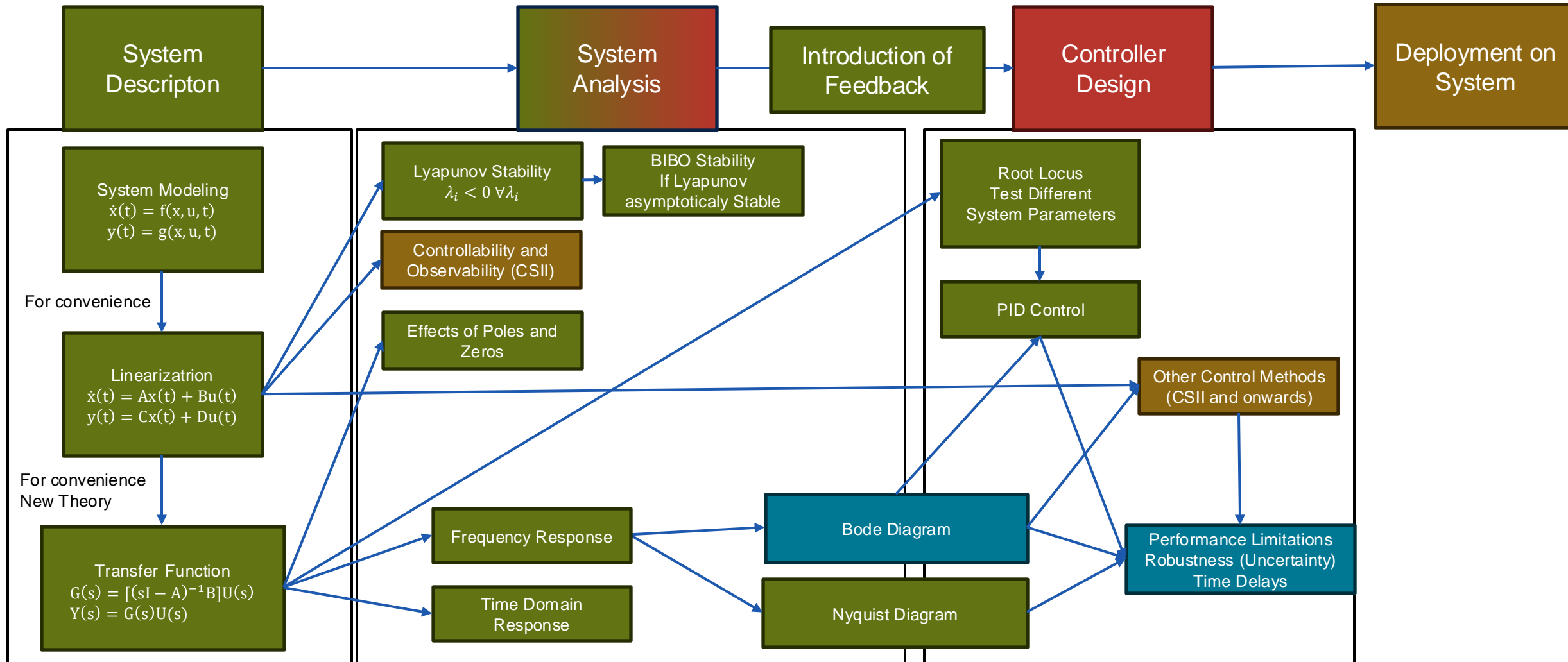
- Sometimes it is just not possible to get all requirements due to nmp zeros or unstable poles
- Rule of thumb on the crossover frequency limits
  - Nominal:  $\max\{10 \cdot \omega_d, 2 \cdot \omega_{p^+}\} < \omega_c < \min\left\{\frac{1}{10} \cdot \omega_n, \frac{1}{2} \cdot \omega_\tau, \frac{1}{2} \cdot \omega_{z^+}\right\}$
  - Conservative:  $\max\{10 \cdot \omega_d, 5 \cdot \omega_{p^+}\} < \omega_c < \min\left\{\frac{1}{10} \cdot \omega_n, \frac{1}{5} \cdot \omega_\tau, \frac{1}{5} \cdot \omega_{z^+}\right\}$
  - $\omega_d$  and  $\omega_n$  are the crossover frequencies of the disturbance and noise
  - $\omega_{p^+}$  and  $\omega_{z^+}$  are the unstable poles and nmp zeros
  - $\omega_\tau = \frac{1}{\tau}$  effect of the time delay (next week)
- If  $\omega_c$  the system can be controlled reasonably (no design specification)

# Outline

- Time Delay
  - What?
  - Effects
  - Example
  - What to do?
  - Approximations
- Controller Design
  - How to implement a controller
- Non-Linearities
- Cascaded Control
  - What?
  - Example

# Conceptual Recap

## Classical Control Approach



# Time Delays

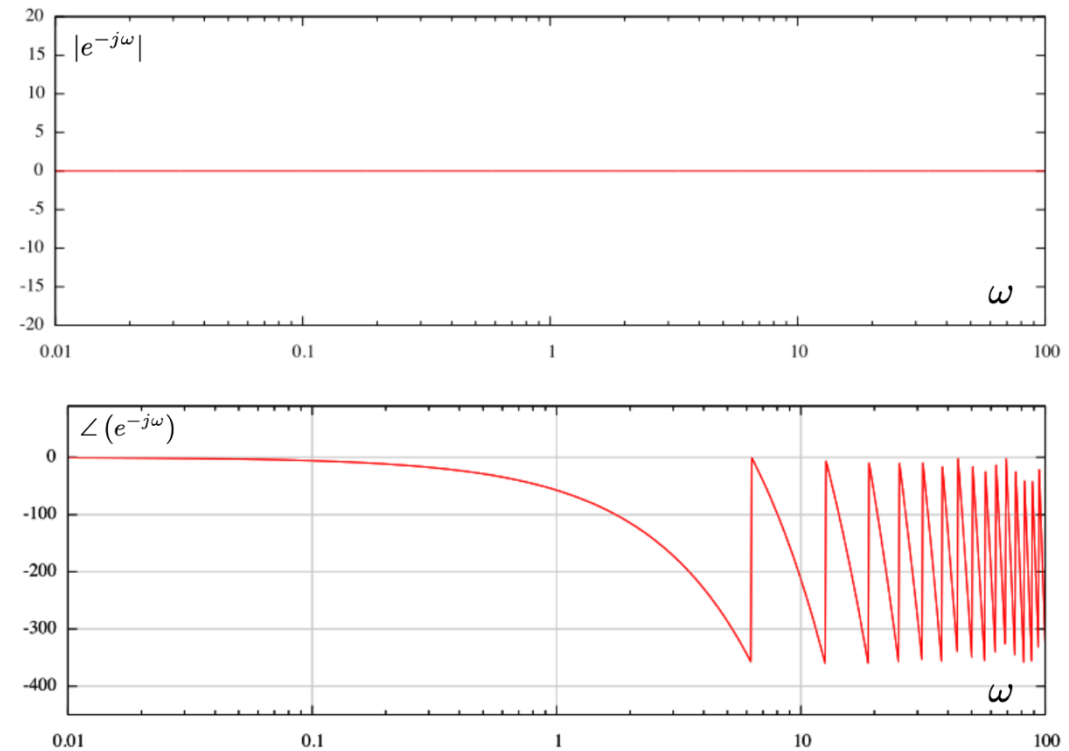
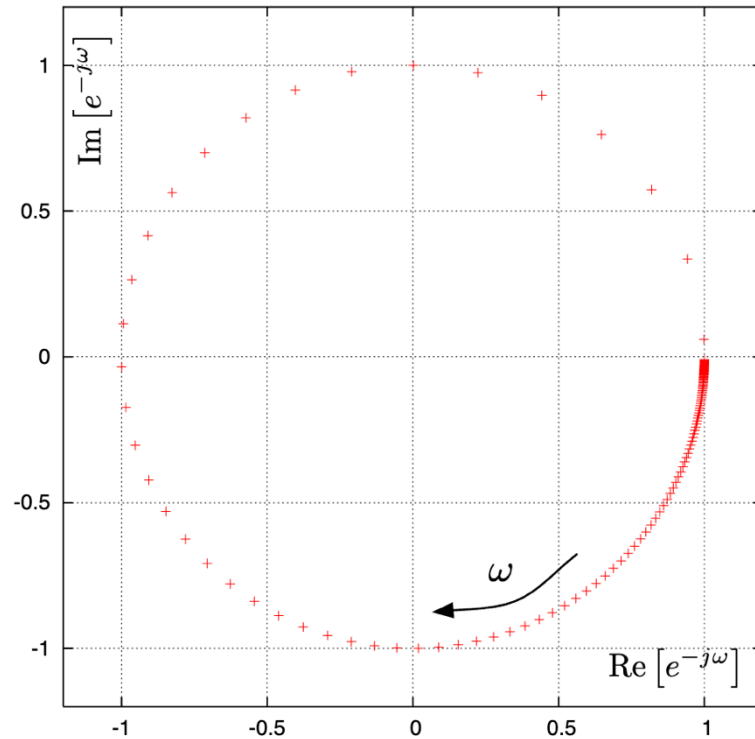
What?

- Whenever an event/transition takes time:
  - Computing a control output using a computer
  - Goods on a conveyor belt with a sensor on the end
  - Long range control (e.g space crafts)
- Definition:
  - A time delay is a **linear** operator that transforms an input signal  $t \rightarrow u(t)$  into a delayed output signal  $y(t) = u(t - T)$ , where  $T \geq 0$  is the delay.
- Transfer Function:
  - $Y(s) = e^{-sT}U(s) \rightarrow G(s) = e^{-sT}$
- Not a polynomial!

# Time Delays

What?

- Transfer Function:
  - $Y(s) = e^{-sT}U(s) \rightarrow G(s) = e^{-sT}$
- Bode Plot and Nyquist Plot:

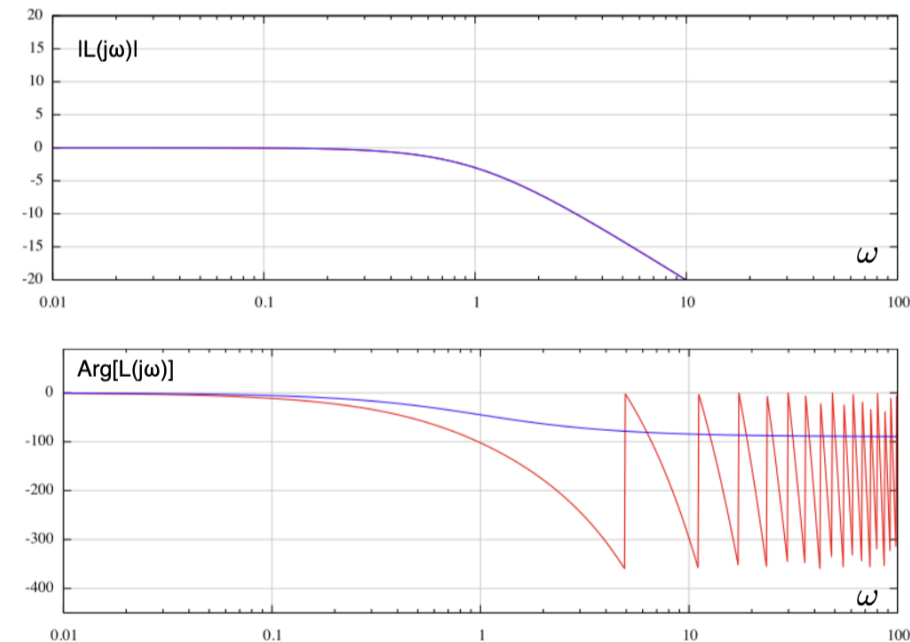
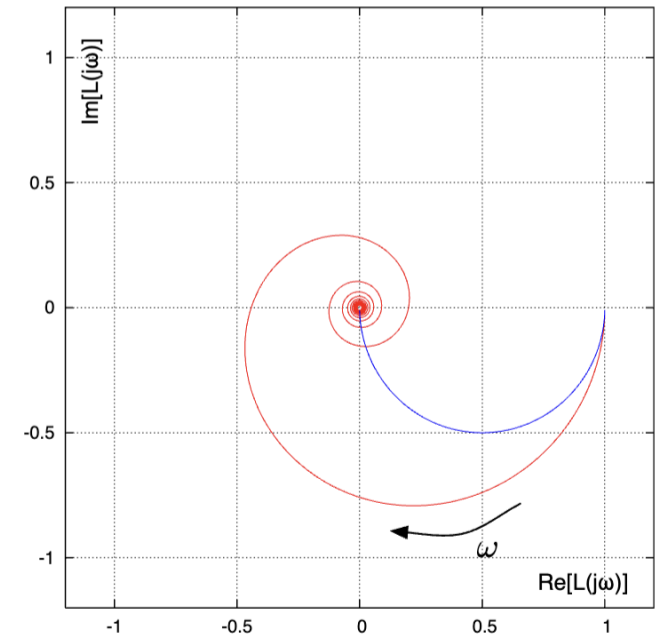




# Time Delays

## Effects

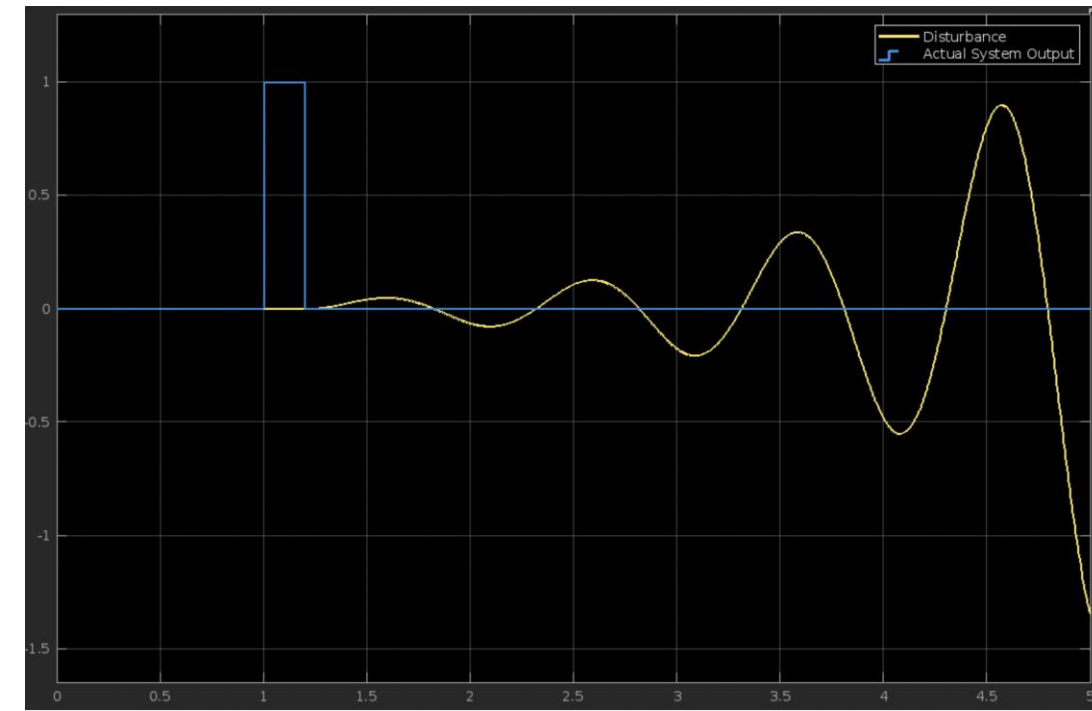
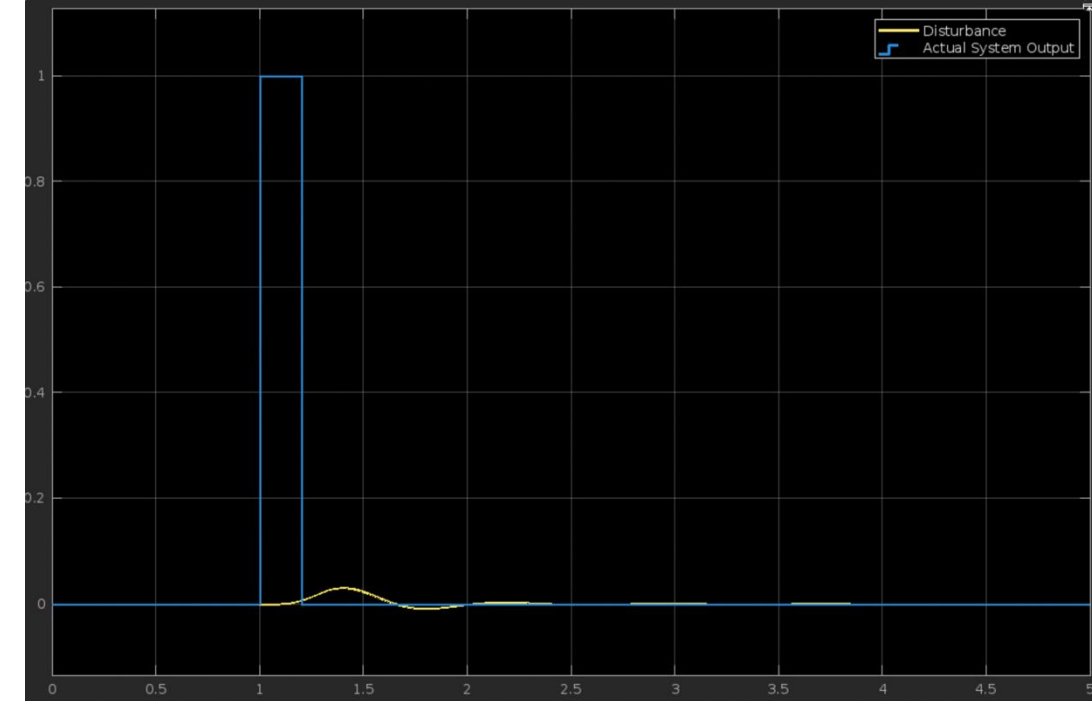
- System with a Time Delay:
  - $L'(s) = e^{-sT}L(s)$
  - $|L'(j\omega)| = |e^{-j\omega T}L(j\omega)| = |L(j\omega)|$
  - $\angle L'(j\omega) = \angle[e^{-j\omega T}L(j\omega)] = \angle L(j\omega) - \omega T, \omega > 0$
- **We lose phase margin!**
  - $\phi_{m,T} = \phi_{m,0} - \omega_c T$
  - Phase margin decrease
  - Decrease is dependent on the cross-over frequency



# Time Delays

## Effects - Example

- Consider the inverted pendulum (upright position):
- $\dot{x} = \begin{bmatrix} 0 & 1 \\ \frac{3g}{2L} & -\frac{3c_f}{mL^2} \end{bmatrix} x + \begin{bmatrix} 0 \\ \frac{1}{mL^2} \end{bmatrix} u, y = [1 \quad 0]x$
- $C(s) = k_p + \frac{k_d s}{T_f s + 1}$ :  $k_p = 35, k_d = 5, T_f = 0.001$
- Plot 1:  $T = 0.1$
- Plot 2:  $T = 0.2$
- Too large of a time delay can make the system unstable
  - Sometimes nothing can help, and we need more sophisticated controllers



# Time Delays

## Example

- Phase margin reduction:

- $\phi_{m,T} = \phi_{m,0} - \omega_c T$

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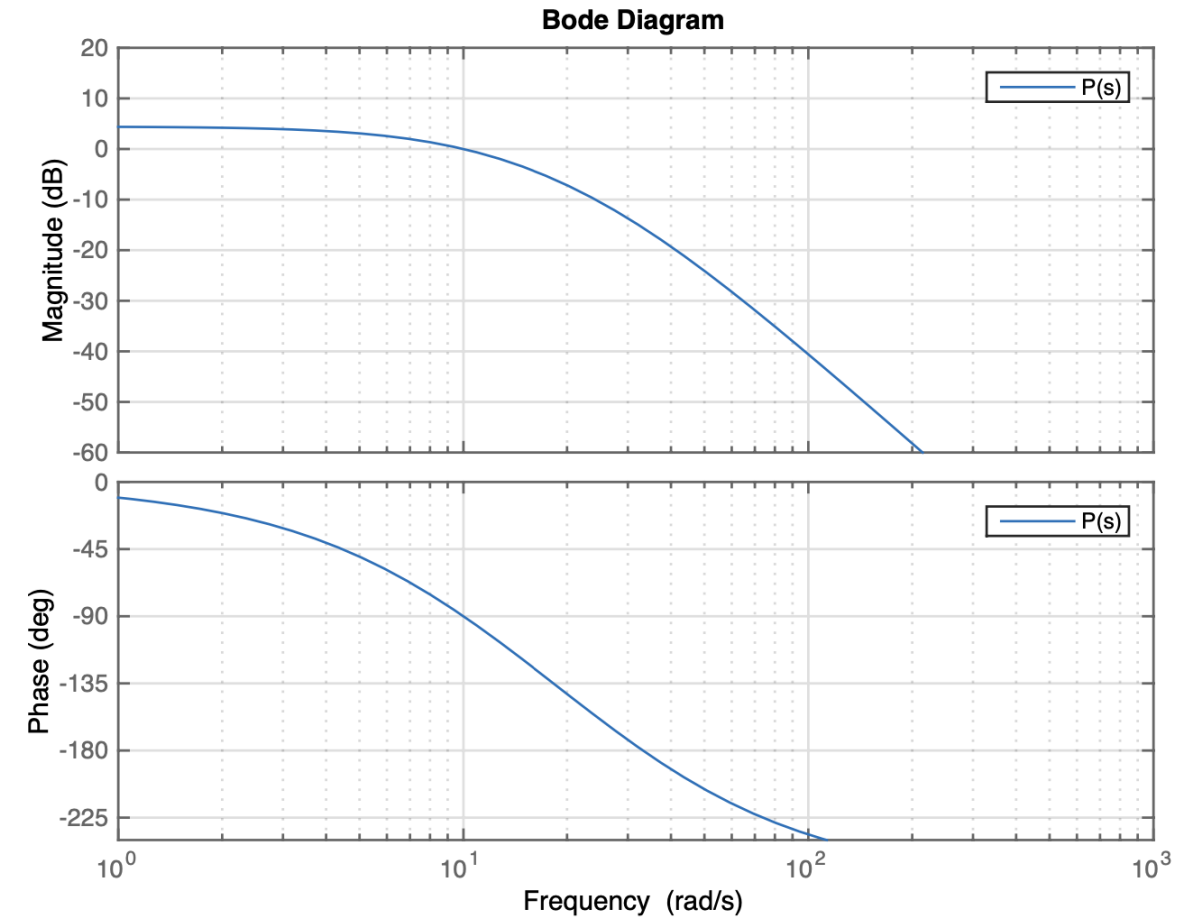
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**Question 45** Choose the correct answer. (1 Point)

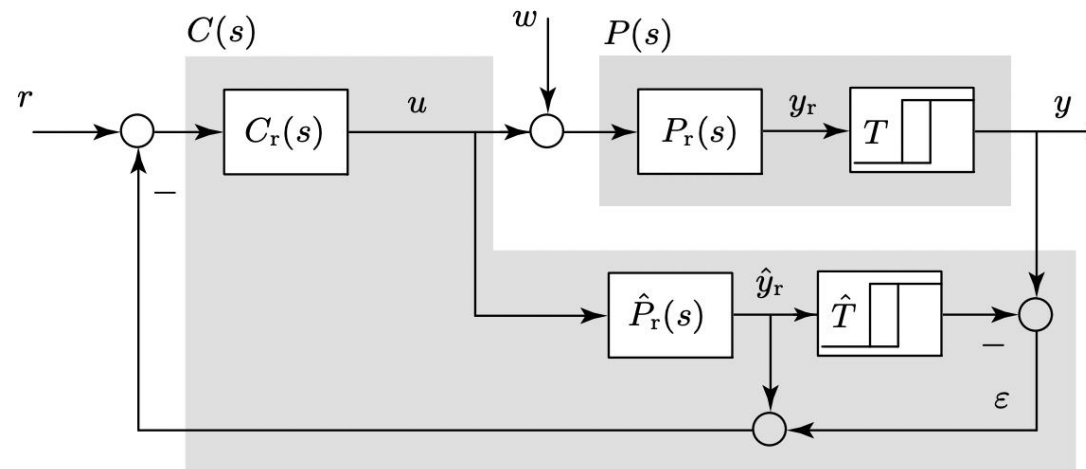
You are given the Bode plot of a plant however the time delay has not been included in the model. You have a time delay of  $T_d = \frac{\pi}{40}$  s. What is the new phase margin/ phase reserve of your system?



# Time Delays

What to do?

- Ignore them and hope for the best
  - Create a controller ignoring the time delay
  - Check the closed loop system:
    - If instable redesign with higher phase margin or lower crossover frequency
  - Repeat until success
- Smith Predictor (not in lecture)
  - Main Idea incorporate time delay knowledge into controller
  - “Simulate” Time Delay in the controller and shift output accordingly



# Time Delays

## Approximations

- Transfer Function is not a Rational Function:
  - $G(s) = e^{-sT}$
  - We can't use root-locus, python or other tools that require rational functions
- Taylor Approximation:
  - $e^{-sT} = 1 - sT + 1/2(sT)^2 - 1/3(sT)^3 + \dots$
  - $e^{-sT} \approx 1 - sT + 1/2(sT)^2$
  - Non-causal with two non-minimumphase zeros -> Only good for  $T \ll 1$
  - Magnitude diverges which is not the case
- Padé:
  - First order:  $e^{-sT} \approx \frac{2/T-s}{2/T+s}$
  - We see the non-minimumphase zeros -> Can't increase gain to much
  - Allows us to do Root-Locus
- For both: Always check with Nyquist for actual stability



# Time Delays

## Approximations - Example

- Consider the Following System:

- $P(s) = 2 \frac{s+1}{s^2+3s+2} e^{-2s} + \frac{1}{s+2} e^{-s}, e^{-sT} \approx \frac{2/T-s}{2/T+s}$

- What would be the first-order Padé approximation?

- - 
  - 
  -

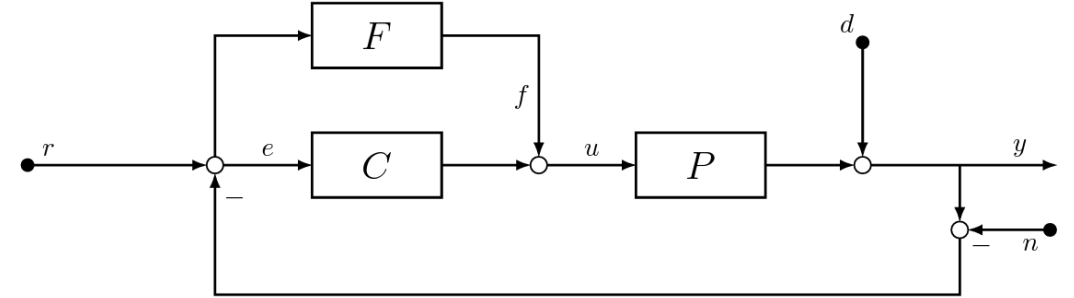
# Controller Design

## How to Implement a Controller

- We saw how to design a controller TF:
  - $C(s) = k + \frac{c_m s^m + \dots + c_0}{s^n + a_{n-1} s^{n-1} + \dots + a_0}$
- We can transfer that to a state space system:

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 & \dots & 0 \\ 0 & 0 & 1 & 0 & \dots & 0 \\ & & \ddots & & & \\ 0 & 0 & 0 & 0 & \dots & 1 \\ -a_0 & -a_1 & \dots & -a_{n-1} & & \end{bmatrix}, \quad B = \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix},$$
$$C = [c_0 \quad c_1 \quad \dots \quad c_{n-1}], \quad D = [d]$$

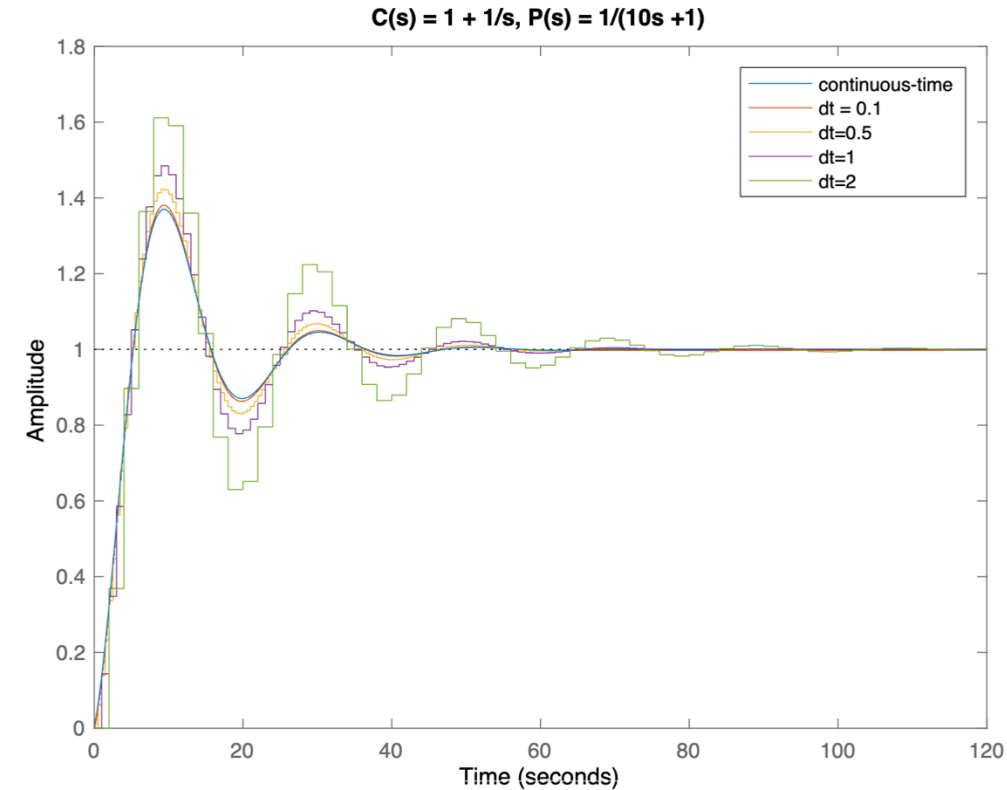
- $\tilde{x}(t) = A\tilde{x}(t) + Be(t), e(t) = r(t) - y(t)$
- $u(t) = C\tilde{x}(t) + De(t)$



# Controller Design

## How to Implement a Controller

- Physical System:
  - Create an Analog Electronics circuit
    - Use Resistors, Capacitors and Inductors
- Software: Euler Approximation (“simulate the controller”)
  - Init  $\hat{x}[k] = 0, e[k-1] = 0$
  - For every  $k$ :
    - $e[k] = r[k] - y[k]$
    - Update system:  $x[k] = x[k] + (Ax[k] + Be[k])dt$
    - Compute output:  $u[k] = Cx[k] + De[k] + K_D(e[k] - e[k-1])/dt$
    - Send  $u[k]$  to actuators
    - Update:  $e[k-1] = e[k]$
  - We keep the output between to step constant -> zero order hold
    - Introduces a time delay of  $dt/2$



# Non-Linearities

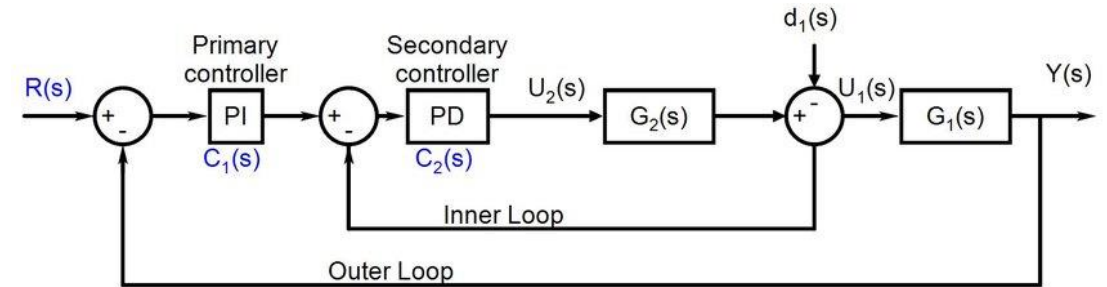
## Linear Systems Theory for Non-Linear Systems

- Most real systems are **non-linear**, but non-linear control theory is hard
- What are the ways to use linear systems theory?
  - Linearization around equilibrium
    - Design a Linear Controller and apply to Non-linear system
      - PID, LQR, Linear MPC
    - Often works well!
    - Stability guarantees only around small deviation of equilibrium!!!
    - Check stability for “expected” deviation or using non-linear systems theory
  - Describing Functions
    - Extend Frequency Domain Methods to non-linear systems
  - Robust Control
    - Create a controller to handle modelling errors and noise

# Cascaded Control

What?

- Split Control Problem into two parts -> Often easier!
  - Low-Level/Inner-Loop(fast) and High-Level/Outer-Loop(slow)
- Low-Level/Inner-Loop : often output of High-Level controller
  - Mostly SISO
  - Often PID/PD
  - Joint Controller, Velocity Controller
- High-Level/Outer-Loop : Used to achieve main goal
  - Often MIMO
  - Usually more complex than a PID/PD
    - MPC, Neural Network, LQR
  - Kinematic Control, Trajectory Following
- Low Level needs to be much faster than High Level!
  - Rule of thumb  $\omega_{LL} \approx 10 * \omega_{HL}$  or  $\omega_{LL} \approx 5 * \omega_{HL}$ 
    - E.g inner loop runs at 300Hz and outer loop at 30Hz

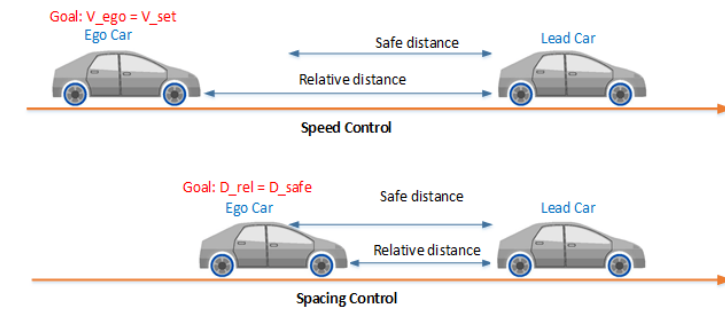
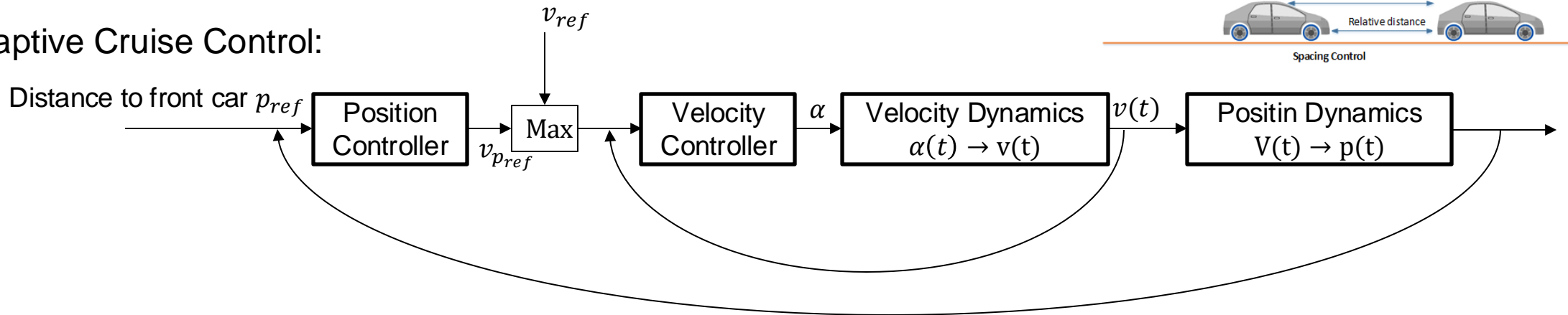




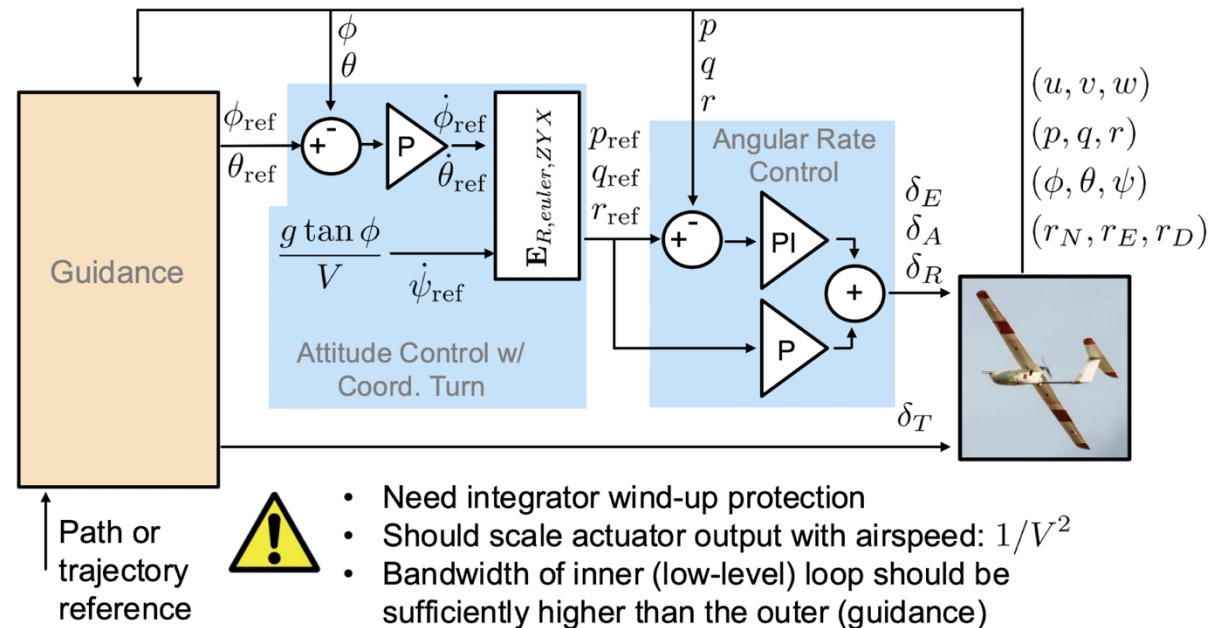
# Cascaded Control

## Examples

### Adaptive Cruise Control:



### Airplane:



# Exercise 10

What to do?

- 1:
  - 1.1 Do
  - 1.2 Do
  - 1.3 Skip
- 2:
  - a) do
  - b) do
  - c) skip
  - d) skip